

Mathematical Interactional Analysis of the Dynamics of Livestock Rearing on the Fertile Topsoil

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Abstract

In this paper a system of deterministic model is presented and analysed to study the potentiality of animal rearing on the organic dynamics of vegetation cover on topsoil. We obtained the effective basic depletion ratio, \mathcal{D}_R , which was used to determine the conditions for the systems local and global stabilities. Bifurcation analysis was carried out using the centre manifold theory which revealed that the model possesses the forward type. Sensitivity analysis showed that the both human and natural activities as well as environmental advocacy campaigns have very similar but varying decrement impacts on vegetation. It is also shown that a sustainable combination of manure harvest and livestock density can improve soil vegetation. It is further shown that the reallocation of soils to non-agricultural purpose also has negative consequence on vegetation.

1.0 Introduction

Animal production (livestock) is globally considered to be done on a greater percentage of agricultural land [1]. In its report, FAO and others outlined the enormous contribution of animal production (livestock) sector to the global agricultural GDP where it is estimated to employ over a billion people apart from being the major source of livelihoods for a billion people, majority of who represent the world's poor [1]. Livestock products are very rich source protein, other essential micronutrients [2]. These nutrients include minerals such as iron and zinc. However, it is being feared that about 925 million of the world's population are seriously undernourished for lack of appropriate and sufficient food supply [3, 4]. Livestock by-products are the major raw materials for a range of essential household products and farm manure [2]. In developing countries for instance, draught animals are estimated to provide 80% of the power used for farming [5]. It is estimated that about 52 percent of draught power comes from animals. In India, selling cattle dung for fuel to urban centres can supply up to 60% of the income of the poor village family. Its prospects in developing countries are bright following its increasing dietary preference over staple food. The number of ruminant animals (like goats and sheep) produced per unit of agricultural area in developing countries is almost double that of undeveloped countries. However, eminent challenges of this on scarce resources such as arable land and water are serious concerns [6]. A high livestock density has implications on soil nutrients and other organic matter content utilization and environmental pollution in addition to the attendant health implication from habitual consumption of a livestock-dominant dietary composition. Furthermore, animal agriculture contributes to greenhouse gas emission in the form of carbon dioxide, methane and nitrous oxide [7, 8] with Africa feared to be worst hit [6]. From the foregoing, an understanding of the ecological and other aspects of animal agriculture is critical to ensure access to safe and healthy food and sustainable environment [9, 10]. Factors influencing animal production and utilisation range from mechanical like farm management and soil condition among others [11, 12, 13, 14]; to biological, which include health, temperature, reproduction and nutrition etc. [15, 16, 17, 18]; and management and socio-economic factors [19, 20, 21]. There is need to simultaneously consider these factors if efficient management systems of animal traction are to be developed [22].

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2.0 Model Formulation and Basic Dynamics of Infertility and Cultivation

The total land mass at time t , denoted by $S(t)$, is classified into two distinct but relatively interrelated soil masses, vegetated topsoil, $S_V(t)$ and the non-vegetated bare land mass, $S_{Nv}(t)$, so that $S(t) = S_V(t) + S_{Nv}(t)$. Animal (cattle, small ruminants and birds) population and their interaction (covering activities like grazing, pecking and burrowing) with vegetated topsoil are modelled by the parameters Φ and η_R respectively. They are reduced by removals (consumption and mortality) at a removal rate, ψ . Soil vegetative cover is assumed to increase at a constant rate Δ , the fractions, λ and ξ respectively monitor human-induced vegetation removals (HIVR) and naturally-induced vegetation removal (NIVR), further, non-agriculture land utilisation (NALU), γ , models (in both classes) soil removals due to developmental (construction) purposes. On the other hand non-vegetated bare land is both increased through a constant recruitment rate Γ and vegetation losses of $S_V(t)$ and then reduced at the rate γ . The assumed removals followed extreme deployable activities on vegetated topsoil. We assume that the stock of manure is accrued either at a constant rate Ω or through animal droppings at a rate λ_R and reduced by application on farmlands at a rate η_B . The deleterious animal-effective-contact rate (AECR), η_P , given by

$$\eta_P = \frac{(\beta_A + \beta_E)S_V + \phi_P\beta_E S_{Nv}}{S}$$

where β_A and β_E are, respectively, the excessive animal and natural effective activity contact rates on S_V and S_{Nv} , sufficient for soil degradation (it is assumed that the severity of this rates increases in the order of their arrangement; thus β_A is milder while β_E is severest); so that as compared with the relative losses on S_V , the modifying parameter, ϕ_P , models increased degradation index on S_{Nv} . The formulation of the present model mimics the flow pattern of epidemiological processes and adopted insights from [23,24].

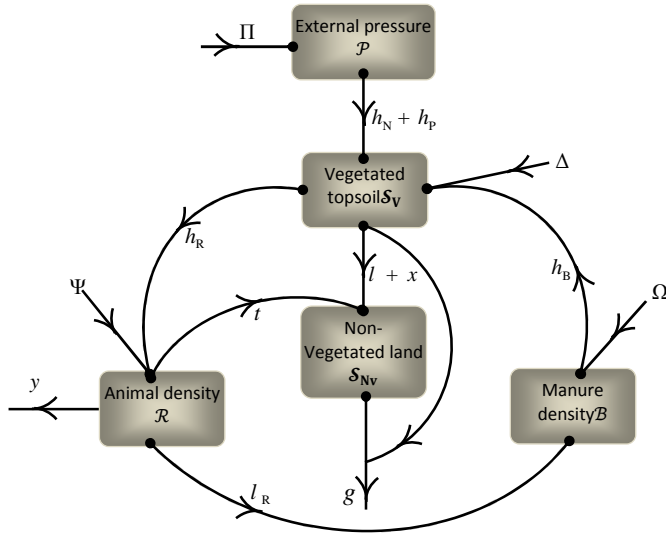


Fig. 1. Model's flow diagram for soil dynamics

2.1 Derivation of Model Equations:

Combining all the aforementioned assumptions and definitions, the model for the dynamics of rearing on a vegetated topsoil is given by the following system of nonlinear differential equations:

$$\begin{aligned} \frac{dP}{dt} &= \Pi - (\eta_P + \eta_N)P \\ \frac{dB}{dt} &= \Omega + \lambda_R R - \eta_B B \\ \frac{dR}{dt} &= \Phi - \psi R \\ \frac{dS_V}{dt} &= \Delta + (\eta_P + \eta_N)P + (\eta_B B + \eta_R R - K_1)S_V \\ \frac{dS_{Nv}}{dt} &= \Gamma + \eta_R R S_{Nv} + (\lambda + \xi)S_V - \gamma S_{Nv} \end{aligned} \tag{1}$$

where $K_1 = \gamma + \lambda + \xi$.

Table 1: Description of model variables

Variable	Description
$\mathcal{P}(t)$	External pressure (both human and natural activities)
$\mathcal{B}(t)$	Aggregate manure
$\mathcal{R}(t)$	Animal population
$\mathcal{S}(t)$	Total land mass
$\mathcal{S}_V(t)$	Mass of vegetated topsoil
$\mathcal{S}_{Nv}(t)$	Mass of non – vegetated land

The densities described by the system(1)are fundamentally nonnegative, thus all variables and parameter values should be nonnegative [24].Thus to verify that the region, Ω , given by $\Omega = \{(\mathcal{P}, \mathcal{B}, \mathcal{R}, \mathcal{S}_V, \mathcal{S}_{Nv}) \in \mathbb{R}_+^5 | \mathcal{S} \leq \Delta/K_1, \mathcal{R} \leq \Phi/\psi\}$, is a positively attracting one for the system (1), we proceed as follows, noting beforehand that the ensuing dynamics of seed and fertile soil densities are

$$\frac{d\mathcal{S}_A}{dt} = \Delta + (\eta_N + \eta_P)\mathcal{P} - K_1\mathcal{S}_A$$

and

$$\frac{d\mathcal{R}}{dt} = \Phi - \psi\mathcal{R}$$

respectively. We note that these densities are particularly maximal whenever $\mathcal{S}_A > \Delta/K_1$ and $\mathcal{R} > \Phi/\psi$ respectively, with the two derivable whenever $d\mathcal{S}_A/dt < 0$ and $d\mathcal{R}/dt < 0$. Since the two rates $d\mathcal{S}_A/dt$ and $d\mathcal{R}/dt$ are respectively bounded by $\Delta - K_1\mathcal{S}_A$ and $\Phi - \psi\mathcal{R}$ applying the standard comparison theorem of Lakshimikantham and Martynyukas used in [24] it can be shown that these solutions hold:

$$\mathcal{S}_A(t) \leq \mathcal{S}_A(0)e^{-K_1t} + \Delta/K_1(1 - e^{-K_1t})$$

and

$$\mathcal{R}(t) \leq \mathcal{R}(0)e^{-\psi t} + \Phi/\psi(1 - e^{-\psi t}).$$

In the same vain, if

$$\mathcal{S}_A(0) \leq \Delta/K_1$$

and

$$\mathcal{R}(0) \leq \Phi/\psi$$

then

$$\mathcal{S}_A(t) \leq \Delta/K_1$$

and

$$\mathcal{R}(t) \leq \Phi/\psi,$$

respectively. Thus each solution of **Error! Reference source not found.**, with initial conditions in Ω , will remain there for all $t > 0$. Thus confirming the positive-invariance and attracting status of Ω . In consequence, therefore, the dynamics of soil infertility could be considered there,since in this region the model (1)can be considered as being agronomically and mathematically well-posed [25].

2.2 Local stability of rearing-free equilibrium (RFE)

The system (1) has an RFE, \mathcal{E}_R , contained in the boundary of \mathbb{R}_+^5 [26] which is gotten by setting the right hand sides of its equations to zero and given by

$$\mathcal{E}_R^0 = (\mathcal{P}^*, \mathcal{B}^*, \mathcal{R}^*, \mathcal{S}_V^*, \mathcal{S}_{Nv}^*) = (\mathbf{0}, \mathbf{0}, \Phi/\psi, \Delta/K_1, \mathbf{0}), \tag{2}$$

The subsystem (1)has an RFE, \mathcal{E}_R^0 contained in the boundary of \mathbb{R}_+^5 [26] obtained by setting the right hand sides of its equations to zero, and given by

$$\mathcal{E}_R^0 = (\mathcal{P}^0, \mathcal{B}^0, \mathcal{R}^0, \mathcal{S}_V^0, \mathcal{S}_{Nv}^0) = (\mathcal{P}^*, \mathcal{B}^*, \mathcal{R}^*, \mathcal{S}_V^*, \mathcal{S}_{Nv}^*), \tag{3}$$

The linear stability of \mathcal{E}_R^0 , can be established using the next generation operator method on the system (3), so that the matrices \mathcal{F} and \mathcal{V} , respectively representing the agronomic terms and all degradative terms, are, respectively given in [27,28]. To simplify our calculation, we evaluate the RFE around the equilibrium $x_0 = (\mathcal{P}^*, \mathcal{B}^*, \mathcal{R}^*, \mathcal{S}_V^*, \mathcal{S}_{Nv}^*)$, to get the matrices

$$\mathcal{F} = \begin{pmatrix} \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \eta_B & \eta_R & \beta_A + \beta_E & \phi_P \beta_E \\ \mathbf{0} & \mathbf{0} & \eta_R & \mathbf{0} & \mathbf{0} \end{pmatrix},$$

And

$$\mathcal{V} = \begin{pmatrix} \eta_N & 0 & 0 & 0 & 0 \\ 0 & \eta_B & -\lambda_R & 0 & 0 \\ 0 & 0 & \psi & 0 & 0 \\ -\eta_N & 0 & 0 & K_1 & 0 \\ 0 & 0 & 0 & -(\lambda + \xi) & \gamma \end{pmatrix}.$$

Thus

$$\mathcal{V}^{-1} = \begin{pmatrix} -\eta_N^{-1} & 0 & 0 & 0 & 0 \\ 0 & -\eta_B^{-1} & \lambda_R/\psi\eta_B & 0 & 0 \\ 0 & 0 & \psi^{-1} & 0 & 0 \\ K_1^{-1} & 0 & 0 & K_1^{-1} & 0 \\ (\lambda + \xi)/\gamma K_1 & 0 & 0 & (\lambda + \xi)/\gamma K_1 & \lambda^{-1} \end{pmatrix}$$

The next generation matrix, $\mathcal{G} = \mathcal{F} \times \mathcal{V}^{-1}$, thus becomes

$$\mathcal{G} = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ \frac{\beta_A + \beta_E}{K_1} + \frac{\phi_P \beta_E (\lambda + \xi)}{\gamma K_1} & 1 & \frac{\eta_R + \lambda_R}{\psi} & \frac{\beta_A + \beta_E}{K_1} + \frac{\phi_P \beta_E (\lambda + \xi)}{\gamma K_1} & \frac{\phi_P \beta_E}{\gamma} \\ 0 & 0 & \eta_R/\psi & 0 & 0 \end{pmatrix}$$

Therefore the spectral radius of the next generation matrix, [27, 28, 29], (respectively with respect to degradation) is

$$\mathcal{D}_R = \frac{\gamma \beta_A + \beta_E [\gamma + \phi_P (\lambda + \xi)]}{\gamma K_1} \tag{4}$$

The following result follows from Theorem 2 of [27]

Lemma 1: *The RFE of rearing on vegetated topsoil model(1), given by(3), is locally asymptotically stable (LAS) if $\mathcal{D}_R < 1$ and unstable if $\mathcal{D}_R > 1$.*

The threshold quantity \mathcal{D}_R as the soil depletion number measures the average of mass of new soil degradation, on a vegetated topsoil land mass, by a typical causative agent [29].

1.1. Analysis of \mathcal{D}_R . The computed threshold quantity is used to determine whether or not rearing on a vegetated topsoil can lead to effective degradation management and consequently improve livestock production. Since all model parameters are positive, it is obvious from (4) that

Theorem 2: *The rearing free equilibrium (RFE) is locally asymptotically stable if $\mathcal{D}_R < 1$.*

Proof: We use the Jacobian stability technique to achieve this claim.

The Jacobian of the system (1) around \mathcal{E}_R^0 is

$$\mathcal{J}(\mathcal{E}_R^0) = \begin{pmatrix} -\eta_N & 0 & 0 & 0 & 0 \\ 0 & -\eta_B & \lambda_R & 0 & 0 \\ 0 & 0 & -\eta_R & 0 & 0 \\ \eta_N & \eta_B & \eta_R & \beta_A + \beta_E - K_1 & \phi_P \beta_E \\ 0 & 0 & \eta_R & \lambda + \xi & -\gamma \end{pmatrix} \tag{5}$$

The row transformed matrix $\mathcal{J}(\mathcal{E}_R^0)$ is as given below

$$\mathcal{J}(\mathcal{E}_R^0) = \begin{pmatrix} -\eta_N & 0 & 0 & 0 & 0 \\ 0 & -\eta_B & \lambda_R & 0 & 0 \\ 0 & 0 & -\eta_R & 0 & 0 \\ 0 & 0 & 0 & \beta_A + \beta_E - K_1 & \phi_P \beta_E \\ 0 & 0 & 0 & 0 & a \end{pmatrix} \tag{6}$$

where

$$a = -\frac{\gamma K_1 - [\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)]}{K_1 - (\beta_A + \beta_E)}$$

Thus the corresponding eigenvalues are:

$$\lambda_1 = -\eta_B, \lambda_2 = -\eta_R, \lambda_3 = -\eta_N, \lambda_4 = \beta_A + \beta_E - K_1,$$

$$\lambda_5 = -\frac{\gamma K_1 - [\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)]}{K_1 - (\beta_A + \beta_E)}$$

Thus $\lambda_4 < 0$ if $K_1 > (\beta_A + \beta_E)$ and $\lambda_5 < 0$ if $\frac{\gamma K_1 - [\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)]}{\gamma K_1 - (\beta_A + \beta_E)} < 1$, provided

The result follows immediately from (4).

2.3 Global stability of RFE

Following the procedure in [30] we establish the global stability of the system (1) as follows: firstly, for emphasis, we reproduce the stability scheme of [30], which can also be looked up in [31].

Theorem 3: Consider a model system that is described by the following differential equations [30]

$$\frac{dx_1}{dt} = \mathcal{F}(x_1, x_2) \tag{7}$$

and

$$\frac{dx_2}{dt} = \mathcal{G}(x_1, x_2); \mathcal{G}(x_1, 0) = 0, \tag{8}$$

where $x_1 \in \mathbb{R}^m, x_2 \in \mathbb{R}^n$ and $x_0 = (x_1^*, 0)$ denote, respectively, the uninfected, infected components of a given populations and the disease- (in this present sense challenged or compromised, that is, infertility) free equilibrium of the system. Assume further that

(H1). For $\frac{dx_1}{dt} = \mathcal{F}(x_1, x_2)$, x_1^* is globally asymptotically stable and

(H2). $\mathcal{G}(x_1, x_2) = \mathcal{A}x_2 - \hat{\mathcal{G}}(x_1, x_2)$, $\hat{\mathcal{G}}(x_1, x_2) \geq 0$ for $(x_1, x_2) \in \Omega$, where the Jacobian $\frac{d\mathcal{G}}{dx_1} = \mathcal{F}(x_1^*, 0)$ is an M-matrix (the off diagonal elements of \mathcal{A} are nonnegative) and Ω is the region where the model makes biological (agronomical) sense. Then the RFE $x_0 = (x_1^*, 0)$ is globally asymptotically stable provided $\mathcal{D}_R < 1$.

From the foregoing we argue as follows:

Theorem 4: The RFE of the model (1) is globally asymptotically stable (GAS) in Ω provided $\mathcal{D}_R < 1$

Proof: Conditions (H1) and (H2), of Theorem 1 above needed to be satisfied for $\mathcal{D}_R < 1$. To achieve this, we deduce from (1) that $x_1 = (\mathcal{P}, \mathcal{S}_{Nv}) \in \mathbb{R}^2$ and $x_2 = (\mathcal{B}, \mathcal{C}, \mathcal{S}_v) \in \mathbb{R}^3$ denote our infertility-free and infertile densities respectively. The RFE is $\mathcal{E}_R^0 = (x_1^0, 0)$, where $x_1^0 = (\Pi/\eta_N, \Gamma/\gamma)$.

Thus by (H1) together with **Error! Reference source not found.** it will become clear that

$$\frac{dx_1}{dt} = \mathcal{F}(x_1, 0) = \begin{pmatrix} \Pi - \eta_N \mathcal{P}^0 \\ \Omega - \eta_B \mathcal{B}^0 \end{pmatrix} \tag{9}$$

Hence

$$\mathcal{P}^0(t) = \frac{\Pi}{\eta_N} - \frac{\Pi}{\eta_N} e^{-\eta_N t} + \mathcal{P}^0(0) \frac{\Pi}{\eta_N} e^{-\eta_N t} \tag{10}$$

and

$$\mathcal{S}_{Nv}^0(t) = \frac{\Gamma}{\gamma} - \frac{\Gamma}{\gamma} e^{-\gamma t} + \mathcal{S}_{Nv}^0(0) \frac{\Gamma}{\gamma} e^{-\gamma t}, \tag{11}$$

Therefore, the mass of soil, when infertility is assumed to be nonexistence is $\mathcal{S}_{Nv}^0 \rightarrow \mathcal{S}^0(0)$ as $t \rightarrow \infty$, irrespective of the values of $\mathcal{P}^0(0)$. Hence x_1^0 is globally asymptotically stable.

Secondly, for $\mathcal{G}(x_1, x_2) = \mathcal{A}x_2 - \hat{\mathcal{G}}(x_1, x_2)$, then we will have that

$$\mathcal{A} = \begin{pmatrix} -\eta_B & \lambda_R & 0 \\ 0 & -\psi & 0 \\ \eta_B & \eta_R & -K_1 \end{pmatrix} \tag{12}$$

Since all the off-diagonal elements of (12) are nonnegative, then \mathcal{A} must be an M-matrix.

$$\mathcal{G}(x_1, x_2) = \begin{pmatrix} \Omega + \lambda_R \mathcal{R} - \eta_B \mathcal{B} \\ \Phi - \psi \mathcal{R} \\ \Delta + [\eta_B \mathcal{B} + \eta_R \mathcal{R} - K_1] \mathcal{S}_v \end{pmatrix} \tag{13}$$

therefore $\hat{\mathcal{G}}(x_1, x_2) = \mathcal{A}x_2 - \mathcal{G}(x_1, x_2) = 0$, since obviously

$$\hat{\mathcal{G}}(x_1, x_2) = (0, 0)^T. \tag{14}$$

Note: this follows from the expression for x_2 as well as the (12) and (13). The proof thus follows.

2.4 Existence of the continuous rearing free (endemic) equilibrium state \mathcal{E}^*

The conditions for the continuous non livestock rearing on vegetated topsoil (the case where not all of $\mathcal{P}, \mathcal{B}, \mathcal{R}, \mathcal{S}_v, \mathcal{S}_{Nv}$), denoted by $\mathcal{E}_R^* = (\mathcal{P}^*, \mathcal{B}^*, \mathcal{R}^*, \mathcal{S}_v^*, \mathcal{S}_{Nv}^*)$, have zero density, a situation derivable when the coordinates of the equations in (1) satisfy the conditions described below:

$$\mathcal{E}_R^* = \{(\mathcal{P}^*, \mathcal{B}^*, \mathcal{R}^*, \mathcal{S}_v^*, \mathcal{S}_{Nv}^*) | \mathcal{P}^* > 0, \mathcal{B}^* > 0, \mathcal{R}^* > 0, \mathcal{S}_v^* > 0, \mathcal{S}_{Nv}^* > 0\} \tag{15}$$

Lemma 5: The continuous non-rearing on vegetated topsoil equilibrium of the model (1) exists whenever the effective depletion ratio, \mathcal{D}_R is greater than unity

Proof: At the persistence equilibrium state, let

$$(\mathcal{P}, \mathcal{B}, \mathcal{R}, \mathcal{S}_v, \mathcal{S}_{Nv}) = (\mathcal{P}^*, \mathcal{B}^*, \mathcal{R}^*, \mathcal{S}_v^*, \mathcal{S}_{Nv}^*) \tag{16}$$

However we note that the expression for \mathcal{D}_R (see (4)) is independent of both manure livestock densities, thus suppressing all traces of the two in the remaining four compartments of (1) gives the following

$$\mathcal{P}^* = \frac{\Pi}{\eta_P^* + \eta_N^*}, \mathcal{S}_V^* = \frac{\Delta + \Pi}{K_1}, \mathcal{S}_{N_V}^* = \frac{K_1 \Gamma + (\lambda + \xi)(\Delta + \Pi)}{\gamma K_1} \quad (17)$$

Substituting (17) in the expression for η_P^* we observe the following:

$$\mathcal{S}^* = \mathcal{S}_V^* + \mathcal{S}_{N_V}^* = \frac{K_1 \Gamma + (\gamma + \lambda + \xi)(\Delta + \Pi)}{\gamma K_1},$$

Thus

$$\eta_P^* = \frac{\phi_P \beta_E K_1 \Gamma + [\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)](\Delta + \Pi)}{K_1(\Gamma + \Delta + \Pi)}$$

or

$$\eta_P^* K_1(\Gamma + \Delta + \Pi) - \phi_P \beta_E K_1 \Gamma - [\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)](\Delta + \Pi) < 0 \quad (18)$$

It can easily be verified that $\frac{[\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)](\Delta + \Pi)}{K_1(\Gamma + \Delta + \Pi)} < \frac{\phi_P \beta_E K_1 \Gamma}{K_1(\Gamma + \Delta + \Pi)}$

which can easily be simplified to give

$$\frac{[\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)](\Delta + \Pi)}{\gamma K_1} < 1 \text{ or } \mathcal{D}_R > 1$$

as required.

Hence the system (1) has a unique positive solution of the form

$$\eta_P^* = \frac{\phi_P \beta_E K_1 \Gamma + [\gamma(\beta_A + \beta_E) + \phi_P \beta_E (\lambda + \xi)](\Delta + \Pi)}{K_1(\Gamma + \Delta + \Pi)}$$

provided $\mathcal{D}_R > 1$. Thus we conclude as follows

Lemma 6. *The system (1) has a unique persistence equilibrium whenever $\mathcal{D}_R > 1$ and none when otherwise*

2.5 Local stability of Persistence Equilibrium

The computational involvement of the procedure for the standard linearization, about the equilibrium, of a system is quite cumbersome and barely mathematically tractable thus making the method unfavourable. We use the manifold theory, described in [32] and reproduced here as Theorem 7, which is evidently most preferred [24]), to establish the local asymptotic stability of the persistence equilibrium.

Theorem 7. Bifurcation Theorem [32]

Consider the general system of ordinary differential equations with parameter ϕ

$$\frac{dx}{dt} = f(x, \phi), f: \mathbb{R}^n \times \mathbb{R} \rightarrow \mathbb{R} \text{ and } f \in \mathbb{C}^2(\mathbb{R}^n \times \mathbb{R}), \quad (19)$$

where 0 is an equilibrium point of the system, that is $f(0, \phi) \equiv 0 \forall \phi$, and assume that:

1. $\mathcal{A} = \mathcal{D}_x f(0, 0) = \left(\frac{\partial f_i}{\partial x_j}(0, 0) \right)$ is the linearization matrix of the system (19) around the equilibrium 0 with f evaluated at zero. Zero is a simple eigenvalue of \mathcal{A} and other eigenvalues of \mathcal{A} have negative real parts;
2. \mathcal{A} has a right and left eigenvectors, \mathcal{W} and \mathcal{V} , respectively; each corresponding to the zero eigenvalue.

Let f_k be the k^{th} component of f and

$$a = \frac{1}{2} \sum_{k,i,j=1}^n v_k w_i w_j \frac{\partial^2 f_k}{\partial x_i \partial x_j}(0, 0) \text{ and } b = \sum_{k,i=1}^n v_k w_i \frac{\partial^2 f_k}{\partial x_i \partial \phi}(0, 0) \quad (20)$$

Then the local dynamics of the system (19) around the equilibrium point 0 is totally determined by the signs of a and b .

- i. $a > 0, b > 0$. When $\phi < 0$ with $|\phi| \ll 1$, 0 is locally asymptotically stable and there exists a positive unstable equilibrium; when $0 < \phi \ll 1$, 0 is unstable and there exists a negative locally asymptotically stable equilibrium;
- ii. $a < 0, b < 0$. When $\phi < 0$ with $|\phi| \ll 1$, 0 is unstable; when $0 < \phi \ll 1$, 0 is a locally asymptotically stable equilibrium, and there exists a positive unstable equilibrium;
- iii. $a > 0, b < 0$. When $\phi < 0$ with $|\phi| \ll 1$, 0 is unstable, and there exists a locally asymptotically stable negative equilibrium; when $0 < \phi \ll 1$, 0 is stable and there exists a positive unstable equilibrium;
- iv. $a < 0, b > 0$. When ϕ changes from negative to positive, 0 changes its stability from stable to unstable. Correspondingly, a negative unstable equilibrium becomes positive and locally asymptotically stable.

Note: if $a > 0$ and $b > 0$ then a backward bifurcation occurs at $\phi = 0$.

To organise our ensuing system for computational convenience, consider the following simplifications and change of variables: let

$$\mathcal{P} = x_1, \mathcal{B} = x_2, \mathcal{C} = x_3, \mathcal{S}_V = x_4 \text{ and } \mathcal{S}_{NV} = x_5 \implies \mathcal{S} = \mathcal{S}_V + \mathcal{S}_{NV} = x_4 + x_5;$$

further, using the vector notation

$$X = (x_1, x_2, x_3, x_4, x_5)^t$$

the subsystem (1) takes the form

$$\frac{dX}{dt} = (f_1, f_2, f_3, f_4, f_5)^t$$

and described as follows:

$$\begin{aligned} \frac{dx_1}{dt} &= f_1 = \Pi - (\eta_P + \eta_N)x_1 \\ \frac{dx_2}{dt} &= f_2 = \Omega + \lambda_R x_3 - \eta_B x_2 \\ \frac{dx_3}{dt} &= f_3 = \Phi - \psi x_3 \\ \frac{dx_4}{dt} &= f_4 = \Delta + (\eta_P + \eta_N)x_1 + (\eta_B x_2 + \eta_R x_3 - K_1)x_4 \\ \frac{dx_5}{dt} &= f_5 = \Gamma + \eta_R x_3 x_5 + (\lambda + \xi)x_4 - \gamma x_5 \end{aligned} \tag{21}$$

Considering γ^* as a bifurcation parameter, then its expression from (4) presently becomes

$$g^* = \frac{f_P b_E (l + x)}{K_1 - b_A - b_E} \tag{1}$$

Note that the above linearised system, of the transformed subsystem (21) with $\gamma = \gamma^*$ has a zero eigenvalue which is simple [24], thus the centre manifold theory can be used to analyse the dynamics of (21) near the chosen bifurcation parameter, [33]. To this end, theorem 4.1 of [32] will be used to show the LAS of the endemic equilibrium point of (1) as transformed in (21) for $\gamma = \gamma^*$

Eigenvectors of $J(\mathcal{E}_R^*)$ at $\gamma = \gamma^*$

Let $W = (w_1, w_2, w_3, w_4, w_5)^t$ and $V = (v_1, v_2, v_3, v_4)$ be the corresponding right and left eigenvectors associated with the zero eigenvalues of the Jacobian J_{γ^*} . Then for:

$$VJ(\mathcal{E}_R^0) = \begin{pmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \\ v_5 \end{pmatrix} \begin{pmatrix} -\eta_N & 0 & 0 & -(\beta_A + \beta_E) & -\phi_P \beta_E \\ 0 & -\eta_B & \lambda_R & 0 & 0 \\ 0 & 0 & -\eta_R & 0 & 0 \\ \eta_N & \eta_B & \eta_R & \beta_A + \beta_E - K_1 & \phi_P \beta_E \\ 0 & 0 & \eta_R & \lambda + \xi & -\gamma \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

Thus the left eigenvalues are

$$v_1 = v_2 = v_4, v_3 = \frac{\lambda_R v_1 + \eta_R (v_4 + v_5)}{\eta_R}, v_1 = \frac{(\beta_A + \beta_E - K_1)v_4 + (\lambda + \xi)v_5}{\beta_A + \beta_E},$$

$$v_5 = \frac{\phi_P \beta_E (v_4 - v_1)}{\gamma} = 0 \implies v_1 = \frac{\beta_A + \beta_E - K_1}{\beta_A + \beta_E} v_4, \text{ and } v_3 = \frac{\lambda_R v_1 + \eta_R v_4}{\eta_R}$$

Similarly, the right eigenvector as computed thus

$$J(\mathcal{E}_R^0)W = \begin{pmatrix} -\eta_N & 0 & 0 & -(\beta_A + \beta_E) & -\phi_P \beta_E \\ 0 & -\eta_B & \lambda_R & 0 & 0 \\ 0 & 0 & -\eta_R & 0 & 0 \\ \eta_N & \eta_B & \eta_R & \beta_A + \beta_E - K_1 & \phi_P \beta_E \\ 0 & 0 & \eta_R & \lambda + \xi & -\gamma \end{pmatrix} \begin{pmatrix} w_1 \\ w_2 \\ w_3 \\ w_4 \\ w_5 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

has the following associated values

$$w_1 = -\frac{(\beta_A + \beta_E)w_4 + \phi_P \beta_E w_5}{\eta_N}, w_2 = w_3 = 0, w_4 = \frac{\eta_N w_1 + \phi_P \beta_E w_5}{K_1 - (\beta_A + \beta_E)}, w_5 = \frac{\lambda + \xi}{\gamma} w_4$$

it thus follows from (6) that if $v_4 > 0$, then $v_1 = v_2 > 0 \implies v_3 > 0$; $v_5 > 0$. Also if $w_4 > 0$, then $w_1 > 0$ and $w_5 > 0$.

Computations of a and b :

Noting that at RFE $\eta_p^* = 0$, then the derivatives of the transformed system (21) are computed thus:

$$\frac{\partial^2 f_1}{\partial x_1^2} = \frac{\partial^2 f_1}{\partial x_1 \partial x_2} = \frac{\partial^2 f_1}{\partial x_1 \partial x_3} = 0, \frac{\partial^2 f_1}{\partial x_1 \partial x_4} = \frac{\partial^2 f_1}{\partial x_4 \partial x_1} - 1, \frac{\partial^2 f_1}{\partial x_1 \partial x_5} = \frac{\partial^2 f_1}{\partial x_5 \partial x_1} = -\frac{\eta_N \phi_P \beta_E}{\Pi}$$

$$\frac{\partial^2 f_4}{\partial x_1 \partial x_4} = \frac{K_1(\beta_A + \beta_E)}{\Delta + \Pi}, \frac{\partial^2 f_4}{\partial x_1 \partial x_5} = \frac{\phi_P \beta_E K_1}{\Delta + \Pi}, \frac{\partial^2 f_5}{\partial x_3 \partial x_5} = \frac{\partial^2 f_5}{\partial x_5 \partial x_3} = \eta_R$$

Then

$$a = \frac{v_1 w_1}{2} \left\{ \frac{K_1}{\Delta + \Pi} [(\beta_A + \beta_E) w_4 + \phi_P \beta_E w_5] - 2 \frac{w_4 \Pi + \eta_N \phi_P \beta_E w_5}{\Pi} \right\}$$

from which it can be verified that

$$a = \frac{v_1 w_1 w_4}{2\gamma} \left\{ \frac{K_1[\gamma(\beta_A + \beta_E) + \phi_P \beta_E(\lambda + \xi)]}{\Delta + \Pi} - \frac{2[\gamma\Pi + \eta_N \phi_P \beta_E(\lambda + \xi)]}{\Pi} \right\} = -1.7426 v_1 w_1 w_4 < 0$$

Similarly, computing for b , with the following derivatives,

$$\frac{\partial^2 f_4}{\partial x_4 \partial \gamma^*} = -1, \frac{\partial^2 f_4}{\partial x_5 \partial \gamma^*} = -1.$$

We have

$$b = -v_4 w_4 < 0$$

Thus, $a < 0, b < 0$. Therefore following Theorem 6, item (ii), we have established the following result (note that this result holds for $\mathcal{D}_R > 1$ but close to 1):

Theorem 8: The unique persistence equilibrium guaranteed by Theorem 7 is LAS for \mathcal{D}_R near 1.

In summary, the model (1) has a globally-asymptotically stable RFE whenever $\mathcal{D}_R < 1$, and a unique persistence equilibrium point whenever $\mathcal{D}_R > 1$. The unique persistence equilibrium point is LAS at least near $\mathcal{D}_R = 1$.

3.0 Numerical Simulation

Table 2. Description of model parameters

Parameter	Description	Baseline value	Reference
D	Natural fertility growth rate of fertile	0.43	Implied from [34]
Ω	Constant manure generation rate	0.3	[35]
F	Animal population	1.3	[34]
Π	Aggregate external pressure rate	10	[36]
g	Soil loss to development	1.77	[34]
l	Soil loss to infertility	2.8	[34]
y	Livestock removal rate	0.1	Assumed
x	Soil loss to erosion	0.75	Assumed
f_P	Modification parameter	0.6	Implied from [34]
h_R	Livestock/soil interaction rate	0.01	Assumed
h_B	Manure decomposition rate	0.75	Assumed
h_N	Soil depletion advocacy rate factor	0.95	Assumed
l_R	Harvested livestock droppings rate	0.35	Assumed
b_A	Anthropological effective contact rate(AECCR)	0.043	[37]
b_E	Erosion effective contact rate(EECCR)	0.263	[37]

In this section, we perform computer simulations to present graphic representations of the results obtained in the immediate section. Pursuant to this, we will use the data presented in table 2, so that the corresponding component values of our positive equilibrium, E_R^* , becomes

$$\mathcal{P}^* = 8.64412, \mathcal{B}^* = 6.46667, \mathcal{R}^* = 13.00000, \mathcal{S}_V^* = 1.10487, \mathcal{S}_{N_V}^* = 2.53799(2)$$

It is found by (23) that condition (4) is satisfied since, as can be verified $\mathcal{D}_R = 0.11700 < 1$ thus by lemma 1 and lemma 2 the RFE of (1) is, both, LAS and GAS, respectively. It can also be verified that by (23) and lemma 5 the RFE has no instance of a continuous non-rearing equilibrium.

To further monitor the effects of the baseline parameters on both topsoil fertility growth and depletion, we herewith present various computer simulations using MATLAB.

Figures 1, 2 and 3 predict the enormous potential of increasing manure decomposition, increased manure harvest and livestock/soil interaction, respectively to support higher vegetation growth on both soil types. This could be due to the expected respective increases in manure deposition and absorption. However, we note that while manure absorption appears to lack the capacity to sustain the gains, probably due to uncontrollable high grazedensity; those of livestock/soil interaction and manure harvest suggest an increasing growth path. We further note the very sharp impact rate of the former as compared to the gradual cases of both interaction and harvest. It can also be observed that when the former began its fall, the other two cases showed an increasing impact.

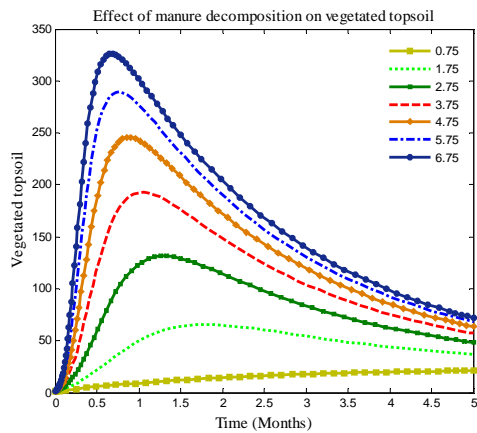


Figure 1a. Plot of vegetated topsoil, S_V , against time for different values of h_B as obtained from Table 2

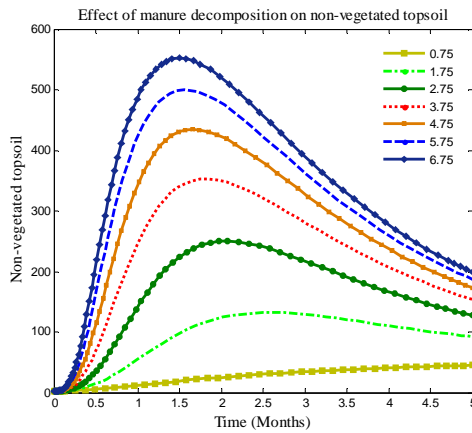


Figure 1b: Plot of non-vegetated topsoil, S_{NV} , against time for different values of h_B as obtained from Table 2

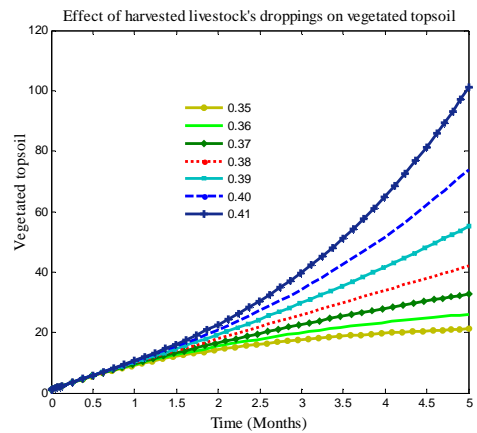


Figure 2a: Plot of vegetated topsoil, S_V , against time for different values of l_R as obtained from Table 2

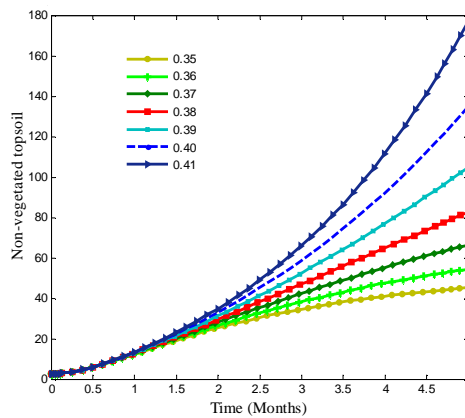


Figure 2b: Plot of non-vegetated topsoil, S_{NV} , against time for different values of l_R as obtained from Table 2

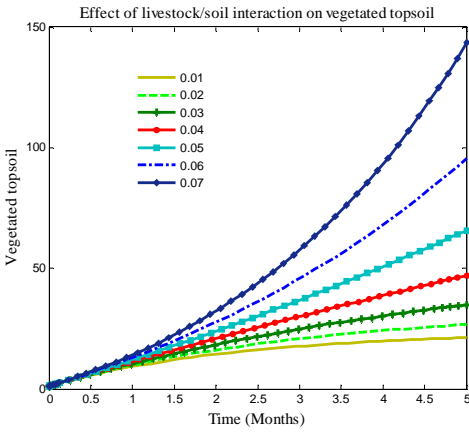


Figure 3a: Plot of vegetated topsoil, S_V , against time for different values of h_R as obtained from Table 2

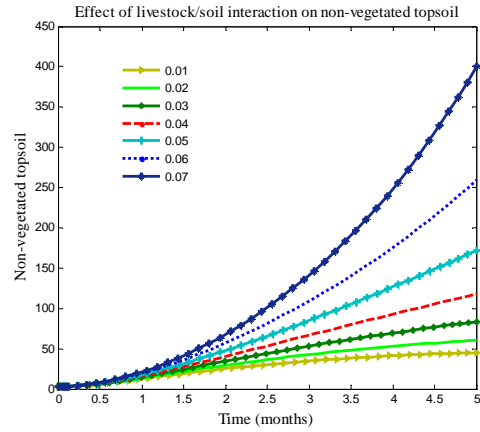


Figure 3b: Plot of non-vegetated topsoil, S_{NV} , against time for different values of h_R as obtained from Table 2

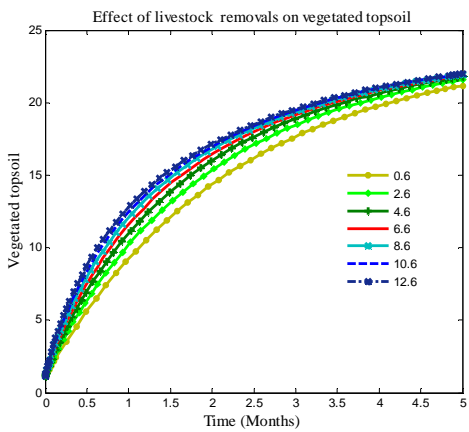


Figure 4a: Plot of vegetated topsoil, S_V , against time for different values of γ as obtained from Table 2

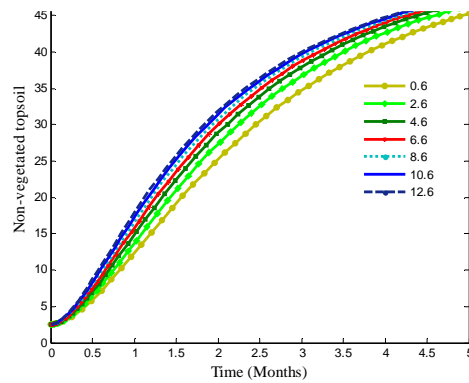


Figure 4b: Plot of non-vegetated topsoil, S_{NV} , against time for different values of γ as obtained from Table 2

Figure 4 on its part suggests that reducing livestock density (either through consumption or death) can increase, though marginally, vegetation growth. In figures 5, 6, 7 and 8 we note that each of human induced vegetation removal (HIVR), natural-induced vegetation removal (NIVR), none agricultural land utilisation (NALU) and environmental enlightenment/advocacy campaigns has the capacity to reduce vegetation growth, the NALU having a substantial impact on non-vegetated topsoil.

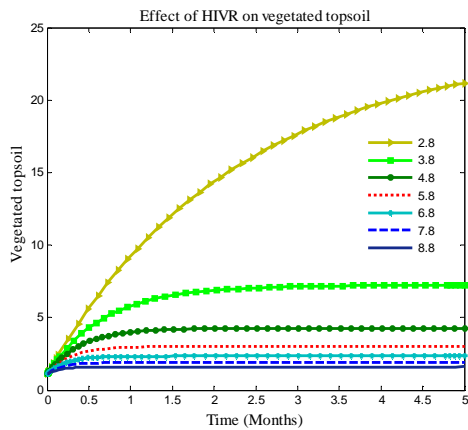


Figure 5a: Plot of vegetated topsoil, S_V , against time for different values of l as obtained from Table 2

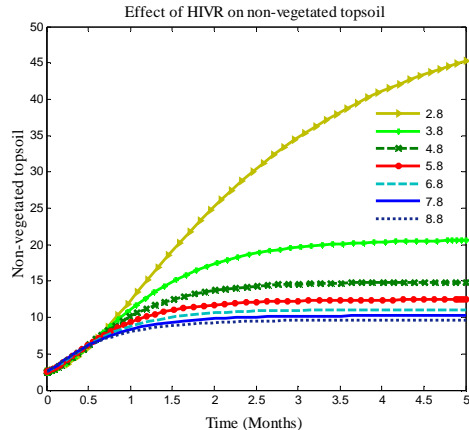


Figure 5b: Plot of non-vegetated topsoil, S_{NV} , against time for different values of l as obtained from Table 2

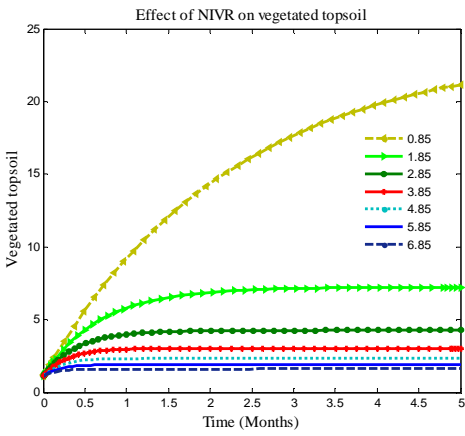


Figure 6a: Plot of vegetated topsoil, S_V , against time for different values of x as obtained from Table 2

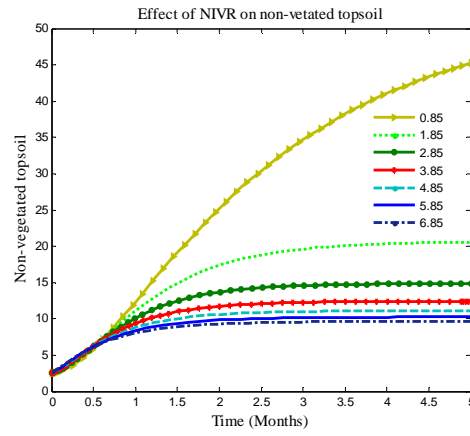


Figure 6b: Plot of non-vegetated topsoil, S_{N_V} , against time for different values of x as obtained from Table 2

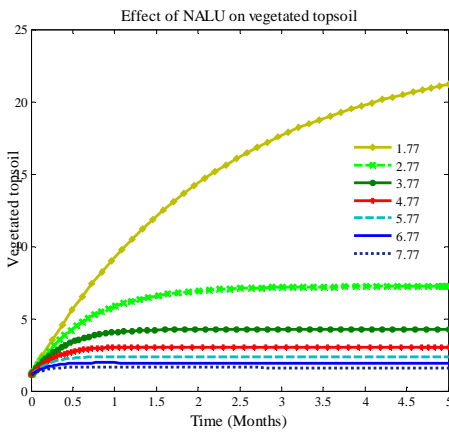


Figure 7a: Plot of vegetated topsoil, S_V , against time for different values of x as obtained from Table 2

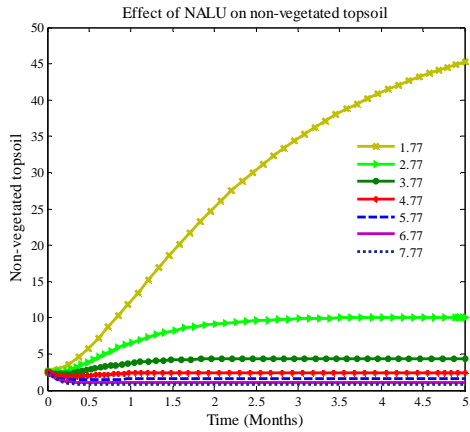


Figure 7b: Plot of non-vegetated topsoil, S_{N_V} , against time for different values of x as obtained from Table 2

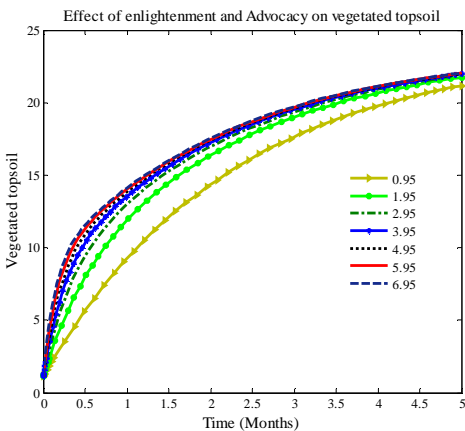


Figure 8a: Plot of vegetated topsoil, S_V , against time for different values of h_N as obtained from Table 2

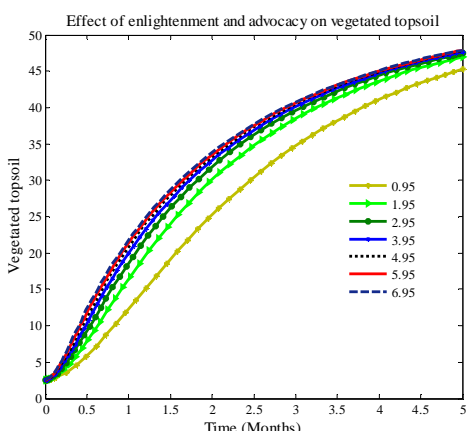


Figure 8b: Plot of non-vegetated topsoil, S_{N_V} , against time for different values of h_N as obtained from Table 2

5.0 Conclusion

In this paper, we presented a system of mathematical model equations to study the impact of organic rearing on fertile topsoil. Extension and other forms of advocacy and enlightenments we found to have positive impact on sustain the environment. To further support this fact, we also showed that when the efforts are excessively deployed on the soil (overgrazing) beyond the sustainable threshold, vegetation cover begin to deplete. The reallocation of soils to NALUs shown to also contribute to vegetation loss. The GAS status of our model implies its global applicability. It has become evidently clear that the first month of the grazing schedule is the most critical. We advocate the simultaneous combination of manure harvest (which could also control wastages), sustainable grazing and sustainable manure disposal (to control excessive ethane and other greenhouse gas emissions).

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