Multi-objective optimal design of a three phase induction motor using geometric programming

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Abstract

This paper presents the use of Geometric Programming optimisation in the optimal design of a three phase induction motor. In order to get the best result we used multiobjective functions with the same constraints. Comparison is made between the independent variables and performance index obtained from these objective functions. The efficiency objective function has the best performance index with efficiency been 95%, power factor 0.87 and torque 47.8 N.m.

Keywords: Geometric Programming, Optimisation, Efficiency, Losses, Power factor Induction Motor, Variables, Constraints, Minimisation, Multi- objective functions, Design.

1.0 Introduction

Three phase induction motors are the most frequently used machines in various electrical drives. About 70% of all industrial loads on a utility are represented by induction motors [1]. The wide applications of induction motors have led to the quest of improving its energy consumption, efficiency and power factor. In the design of induction motors, minimization of certain parameters leads to the production of better and efficient energy saving motors. The optimal design of an induction motor is mainly a proper sizing technique which is subject to a set of constraints. These constraints could be thermal, mechanical or users specifications [1]. Optimization is a science of determining the best solution to certain mathematically defined problems, which are often models of physical reality. Optimization involves the setting up of an, or a set of objective function(s) and making it or these to reach a maximum or minimum value(s) while keeping all variables within an acceptable limit or range. The objective function of an induction motor could be the efficiency [2-3], stator, rotor, iron losses or a combination of two or all the losses [4], cost of material [5] or the torque [6]. Several optimization techniques can be used in solving multi-objective functions derived from an induction motor subject to its stated constraints. Most of the expressions used in the formulation of the objective functions for induction motors are nonlinear and this has prompted some authors [4,7] to solve these objective functions using nonlinear optimization techniques. Some optimization techniques that have been applied in the design of induction motor are, the Genetic Algorithm [4,7-10], the Finite Element Method [11-12], the Particle Swarm optimization[13], and Simulated annealing[14]. All these aforementioned non linear optimization technique has been found to yield good results, and most of them can detect if the solution to the problem is feasible or infeasible at the early stage of the simulation process.

The aim of this paper is to use the Geometric Programming technique in the optimal design of a three phase induction motor using five objective functions namely the maximization of the Efficiency, minimization of the Stator Copper loss, Rotor Copper Loss, Stator Iron loss and the Cost of Material, with the improvement in efficiency, and power factor in mind. The Geometric Programming technique has been proved successful in the cost minimization of transformers [15] and

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synchronous motors [16]. A comparison is performed on these objective functions and the best of the five is sorted out. The condition for selecting the best is the improvement in efficiency, torque, power factor and reduction in cost of production. These are termed the performance index. The performance indexes are derived from the independent variables which are the sizing parameters.

The paper is organised as follows; section 2 sets out the optimization problem which includes the design variables and objective functions. Section 3 outlines a basic review on Geometric programming, section 4 deals with the design of an induction motor using GP, section 5 indicates the optimisation results and discussion, and we conclude in section 6.

2.0 **Optimization Problem**

2.1 Design Variables

The following quantities are chosen as the independent design variables for the multi-objective optimization: Stator bore diameter D, Stator tooth width W_{st} , Rotor tooth width W_{rt} , Depth of stator slot d_{ss} , Depth of stator core d_{sc} , Depth of rotor slot d_{rs} , air gap length l_g , Stator outer diameter D_o , Stator axial length L

2.2 Limits of Variables

The design carried out is for a 7.5 kW, three phase induction motor operating under a 380 Volts, 50 Hz power supply. The minimum and maximum value limits of the independent variables are as shown in table I.

independent variables						
	V	Values (m)				
	min	max				
D	0.1200	0.1500				
W _{st}	0.0045	0.0065				
d_{ss}	0.0160	0.0190				
W _{rt}	0.0035	0.0050				
d_{rs}	0.0160	0.0185				
d_{sc}	0.0280	0.0320				
L	0.1400	0.1900				
l_g	0.0035	0.0050				
D _o	0.1800	0.2200				

Table I: Minimum and maximum limits of

Table II: Nomenclature					
Nomenclature	Meaning				
$ ho_{fe}$	mass density of iron				
K _{fe}	cost of iron per kg				
ρ_{cu}	electrical resistivity of copper				
K _{cu}	cost of copper conductor per kg				
Ν	number of turns per phase				
Ι	stator phase current				
m	number of phase				
J	stator current density				
d_b	depth of rotor bar				
w_b	width of rotor bar				
S_r	number of rotor slots				
a_e	cross section of end ring				
D_e	mean diameter of end ring				
S_s	number of stator slots				
p	number of poles				
L_b	length of rotor bar				

2.3 **Objective Function**

In this work the following objective functions to be maximized or minimized are considered; 1) Material Cost C_M , 2) Stator Copper Loss W_{scu} , 3) Rotor Copper Loss W_{rcu} , 4) Stator Iron Loss W_{sfe} and 5) Efficiency of motor η .

2.3.1 Material Cost

The material cost C_M considered here are those that have direct bearing with the independent variables. These are the cost of iron C_{fe} and copper C_{cu} . The total cost of material is,

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$$C_M = C_{fe} + C_{cu} \tag{1}$$

The cost of iron C_{fe} is given as,

$$C_{fe} = \rho_{fe} K_{fe} (Ld_{cs} \pi (D + 2d_{ss} + d_{cs}) + S_s W_t d_{ss} L)$$
(2)

and the cost of copper C_{cu} (stator winding and rotor bars including end rings) is given as,

$$C_{cu} = \rho_{cu} K_{cu} \left(\frac{NIm}{J} \left(2L + \frac{2.3\pi D}{p} + 0.24 \right) + d_b w_b L_b S_r + 2a_e \pi D_e \right)$$
(3)

Table II contains all the symbols used in 1,2 and 3 and their corresponding meaning

2.3.2 Stator Copper Loss

The stator copper loss W_{scu} is given as,

$$W_{scu} = \rho_{cu} mNJI \left(2L + \frac{2.3\pi D}{p} + 0.24 \right)$$
(4)

2.3.3 Rotor Copper Loss

The rotor copper loss Rotor Copper Loss
$$W_{rcu}$$
 is given as,

$$W_{rcu} = \rho_{cu} (2mk_w NI)^2 \left(\frac{L_b}{S_{rwb}d_b} + \frac{2D_e}{\pi p^2 a_e}\right)$$
(5)

2.3.4 Stator Iron Loss

The stator iron loss W_{sfe} is given as,

$$W_{sfe} = \rho_{fe} \Big(s_s W_{st} L d_{ss} k_1 f^{k_2} B_{st}^{k_3} + \pi (D + 2d_{ss} + d_{sc}) d_{sc} L k_1 B_{sc}^{k_3} f^{k_2} \Big)$$
(6)

where, W_t is the width of stator teeth, k_1 core iron parameter, k_2 core iron constant, k_3 core iron constant, f is power utility frequency, B_{st} is the tooth flux density, B_{sc} is the stator core flux density.

2.3.5 Efficiency

The efficiency η of a machine is given as,

$$\eta = \frac{P_{out}}{P_{out} + W_{cu} + W_{sfe}} \tag{7}$$

The overall copper losses W_{cu} occurring in the stator and rotor slots of a three phase induction motor is given as

$$W_{cu} = \rho_{cu} \left(mNJ \left(2L + 2.3\pi \frac{D}{p} + 0.024 \right) I + (2mNk_w I)^2 \left(\frac{L_b}{s_s d_b w_b} + \frac{2D_e}{\pi p^2 a_e} \right) \right)$$
(8)

where, k_w is the winding factor.

$$\eta = \frac{P_{out}}{P_{out} + \rho_{cu} \left(mNJ \left(2L + 2.3\pi \frac{D}{p} + 0.024 \right) I + (2mNk_w I)^2 \left(\frac{L_b}{ssd_b w_b} + \frac{2D_e}{\pi p^2 a_e} \right) \right) \cdots} + \rho_{fe} \left(s_s W_{st} L d_{ss} k_1 f^{k_2} B_{st}^{k_3} + \pi (D + 2d_{ss} + d_{sc}) d_{sc} L k_1 B_{sc}^{k_3} f^{k_2} \right)}$$
(9)

2.4 Constraints

The following equality and inequality constraints shown in table III are imposed on the optimization problem. These constraints are so chosen so as to bring the best in the design. All the objective functions were subjected to these same constraints.

Table III: Constraints				
constraints				
equality	inequality			
D/2p = dss	$D + 2d_{ss} + 2d_{cs} \le D_o$			
(0.95Wt Ss)/Sr = Wrt	1.15Ss $Wt/\pi p \le dcs$			
$k\pi D/p = L$	$D_r + 2l_g \le D$			
$(\pi DBg)/(1.7Ss) = Wt$	$0.0002 + 0.002\sqrt{DL} \le l_g$			
$Pp/(2.22f\pi^2 Bg D^2 kw Q) = L$	$Q\pi D/(2mI) \le N$			

3.0 Overview of Geometric Programming

A geometric programme (GP) is an optimisation problem of the form [17-20], minimise $f_0(x)$

subject to
$$f_i(x) \le 1$$
 $i = 1, ..., m$,

$$g_i(x) = 1, \quad i = 1, \dots, p.$$
 (10)

where f_i are posynomial functions, g_i are monomials, and x_i are the optimisation variables.

A monomial function is defined as,

$$g_i(x) = c_i x_1^{a_1} x_2^{a_2} \cdots x_n^{a_n}$$
(11)

where *c* is a positive real constant called the monomial coefficient, and $a_{1,\dots,n}a_n$ are real and may be negative or fractional constants that are referred to as the exponents of the monomial.

The sum of monomial functions is named a posynomial function; that is,

$$f_i(x) = \sum_{k=1}^K c_k x_1^{a_{1k}} x_2^{a_{2k}} \cdots x_n^{a_{nk}}$$
(12)

If a posynomial is multiply by a monomial the result is a posynomial, similarly a posynomial can be divided by a monomial with the result being a posynomial.

The geometric programming technique has many similarity to linear programming but has advantage over it in that, a nonlinear objective function can be used, the constraints can be non-linear and the optimal value can be determined with a dual without first determining the specific value of the primal variables [22]

4.0 Design of Induction Motor using GP

In this design the geometric programming (GP) is used in the design of a three phase induction motor whose parameters are as presented in table IV. It is used in finding a set of design variables which ensure that the objective function $f_0(x)$ has a minimum or maximum value and all the constraint are satisfied.

Tuble IV. Motor specification and design constants						
Motor specification			Design Constants			
Power rating (kW)	7.5	k_1 1.9 × 10 ⁻³				
Voltage (V)	380	k_2	1.24			
frequency (f)	50	k_3	2			
No. of poles	4	ρ_{cu}	$1.72 \times 10^{-3}\Omega - cm$			
		$ ho_{fe}$	$4800 kg/m^{3}$			
		K _{fe}	1000/kg			
		κ _{cu}	500/kg			

Table IV: Motor specification and design constants

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5.0 **Results and Discussions**

The results of the design using the multi-objective functions are shown in table V. From the table the following are noted. The independent variables obtained from the simulations are within the minimum and maximum limits. The size of the induction motor is almost the same as shown from the value of the stator outer diameter. The air gap length is within the limit apart from that obtained from W_{sfe} . The higher efficiencies and hence the low losses seen in C_m , W_{rcu} , and η is due to a low depth of the rotor slots. In all the results of the independent variables obtained from the efficiency and rotor copper loss objective functions gives improved performance indexes. From the results obtained the efficiency objective function is the best of the five though the rotor loss objective function shows improve power factor and low cost of materials its computed torque is lower than the calculated torque (47.7 N.m)

Table V: Optimal design results with various objective functions								
Variables/indices	C _M	W _{scu}	W _{rcu}	W _{sfe}	η			
Independent Variables								
Stator bore diameter $D(m)$	0.1321	0.1306	0.1467	0.1321	0.1343			
Stator outer diameter $D_o(m)$	0.2097	0.2152	0.2200	0.2106	0.2179			
Stator tooth width W_{st} (m)	0.0021	0.0034	0.0029	0.0024	0.0034			
Rotor tooth width $W_{rt}(m)$	0.0024	0.0030	0.0026	0.0021	0.0042			
Depth of stator core $d_{sc}(m)$	0.0151	0.0233	0.0183	0.0165	0.0240			
Depth of stator slot $d_{ss}(m)$	0.0165	0.0163	0.0183	0.0165	0.0168			
Depth of rotor slot $d_{rs}(m)$	0.0081	0.0047	0.0183	0.0082	0.0108			
Stator axial length $L(m)$	0.1557	0.1538	0.1728	0.1557	0.1582			
Air gap length $l_a(m)$	0.0056	0.0051	0.0050	0.0056	0.0050			
Dependent variables								
Stator current density $J_s(A/m^2)$	2.7×10^{6}	1.2×10^{6}	2.68×10^{6}	2.68×10^6	1.2×10^{6}			
Rotor current density $J_r(A/m^2)$	5.6×10^{6}	5.6×10^{6}	4.5×10^{6}	5.6×10^{6}	4.5×10^{6}			
Gap flux density $B_g(Wb/m^2)$	0.4716	0.5000	0.3796	0.3500	0.3857			
Performance Index								
Full load efficiency	0.7898	0.8578	0.9373	0.8080	0.9476			
Full load power factor	0.9990	0.9988	0.9371	0.9977	0.8694			
Full load torque (N, m)	41.55	66.2	45.00	31.83	47.80			
Rotor Losses (W)	1709	980.59	184.28	1451	123.5			
Stator losses (W)	247.29	208.24	234.67	292.65	232.75			
Iron losses (W)	41.09	54.39	57.97	37.98	58.300			
Cost (Naira)	7458.5	11551	11198	8100.7	11279			

6.0 Conclusion

The geometric programming optimisation process has been applied on five objective functions namely, Material Cost C_M , Stator Copper Loss W_{scu} , Rotor Copper Loss W_{rcu} , Stator Iron Loss W_{sfe} and Efficiency of motor η in the design of a three phase induction motor with the task of maximizing the efficiency and power factor of the motor. The optimization leads to the determination of the stator and rotor geometry under certain constraining conditions. The results of the stator and rotor geometry variables obtained from the optimization are within the specified limits. As shown in Table IV, the independent variables and performance indexes obtained from the efficiency objective function are the best.

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